



# Reaction to fire test report

Test standard: Ad-hoc test based off ISO 13785-1:2002 Test sponsor: Cladding Safety Victoria (CSV) System: A cassetted aluminium composite panel wall system Job number: RTF230111 Test date: 13 September 2023 Revision: R3.0



## **Quality management**

Revision	Date	Information about the report			
R3.0	R3.0 18 October 2023	Description	Initial issue		
			Prepared by	Reviewed by	Authorised by
		Name	Anthony Rosamilia	Mandeep Kamal	Steven Halliday
		Signature	R	Tekamel.	filling

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## 1. Introduction

This report documents the findings of the third of three ad-hoc reaction to fire tests on a cassetted aluminium composite panel (ACP) external wall system - performed on 13 September 2023. The test was based on ISO 13785-1:2002.

Warringtonfire performed the test at the request of the test sponsor listed in Table 1.

#### Table 1Test sponsor details

Test sponsor	Address	
Cladding Safety Victoria	717 Bourke Street Docklands VIC 3808	
	Australia	

## 2. Test specimen

## 2.1 Schedule of components

Table 2 describes the test specimen and lists the schedule of components. These were provided by the representatives of the test sponsor and surveyed by Warringtonfire. All measurements were done by Warringtonfire – unless indicated otherwise.

Detailed drawings of the test specimen are provided in Appendix A.

#### Table 2 Schedule of components

Item				
nem	Description			
Cladding				
1.	Item name	ACP Panelling - cassetted		
	Product	Econ Panel <sup>™</sup> - 3 mm Glossy White/Matte White(BC-03E) with 0.21 mm skin		
	Manufacturer/Supplier	SAS Signage		
-	Material	The material was nominated as panels consisting of two layers of aluminium sheets sandwiching a layer (core) with 45 % polyethylene (PE) with inorganic filler. Analysis conducted by the analytical centre of UNSW showed that the core consisted of polyethylene-vinyl acetate (PEVA) - found to be 49.8 % w/w - whilst the remainder of the material was found to be 40.2 % calcium carbonate, 7.9 % other inert material and 2.1 % magnesium hydroxide.		
		Refer to Appendix C for more detailed results - Sample 23139-3, CSV #4.		
	Size	As shown in Figure 7.		
		Total thickness – 3.1 mm		
		Skin thickness (both sides) – 0.2 mm		
		Cassette depth – 150 mm		
	Measured mass/unit area densities	Panel areal density – 4.8 kg/m²		
2.	Item name	FR Plasterboard		
	Product	CSR Gyprock 13 mm Fyrchek		
	Manufacturer/Supplier	CSR Gyprock		
	Size	Measured board: 3000 mm × 1200 mm × 13 mm		
	Batch Date:	16/08/22		
	Areal density (measured)	11.0 kg/m <sup>2</sup>		
3.	Item name	Backpan		

ltem	Description		
	Product	0.9 mm thick Galvabond steel	
	Supplier	BlueScope	
	Size	Measured: 1160 mm wide × 3700 mm tall, 0.9 mm thick – in segments	
Frami	ng		
4.	Item name	Test rig frame - 90 × 90 SHS and 200 × 90 PFC frame	
	Size	90 mm × 90 mm × 5 mm thick and 200 mm × 90 mm × 10 mm thick – refer to Figure 6.	
5.	Item name	Aluminium curtain wall transom/mullions (rectangular hollow sections) - framing	
	Size	65 mm wide × 120 mm deep × 3 mm thick Total frame size: 120 mm deep × 1165 mm wide × 3705 mm tall	
	Manufacturer/Supplier	Capral Aluminium	
6.	Item name	Aluminium angles - framing	
	Size	20 mm wide × 30 mm deep × 3 mm thick	
	Manufacturer/Supplier	Rapid Aluminium	
7.	Item name	Aluminium stiffener - framing	
	Size	3 mm thick	
	Manufacturer/Supplier	Rapid Aluminium	
8.	Item name	Internal side frame - steel	
	Size	Studs and noggings: 90 mm deep × 36 mm wide × 0.55 BMT	
	Installation	The steel framing members were riveted (item 17) to one another.	
9.	Item name	Strap – 50 mm wide	
	Size	Studs and noggings: 90 mm deep × 36 mm wide	
	Installation	The steel framing members were riveted (item 17) to one another.	
Smoke	e seal		
10.	Item name	Smoke seal	
	Size	1 mm thick galvanised steel	
	Manufacturer/Supplier	Atlas Steel	
Insula	tion		
11.	Item name	90 mm thick polyethylene terephthalate (PET) insulation	
	Density	10 kg/m <sup>3</sup>	
	Manufacturer/Supplier	Pricewise Insulation	
12.	Item name	50 mm thick aluminium - with fibre-glass mesh - foil faced rockwool insulation	
	Density of core	40 kg/m <sup>3</sup>	
	Manufacturer/Supplier	Rockwool Insulation Australia	
Sealar	nt/Adhesive		
13.	Item name	Weathering sealant	
	Product type	Silicone sealant	
	Product name	PROSIL 41Im	
	Manufacturer/Supplier	Admil Adhesives	

ltem	Descrip	ription		
	Usage		Placed at ACP edges and over screw and rivet locations.	
Fixing	S			
14.	Item name		Wafer head screws – zinc coated steel	
	Size		10g × 16 mm long	
	Installat	tion	Used to fix aluminium angles (item 6) to the aluminium frame (item 5) at 500 mm centres	
15.	Item na	me	Wafer head screws – zinc coated steel	
	Size		10g × 50 mm long	
	Installat	tion	Used to fix ACP (item 1) to the aluminium stiffener (item 7) – four per corner.	
16.	ltem na	me	Hex head tek screw – zinc coated steel	
	Size		12g × 16 mm long	
	Installat	tion	Used to fix aluminium stiffeners (item 7) to themselves	
17.	ltem na	me	Steel rivets	
	Size		Ø4 mm	
18.	ltem na	me	Plasterboard screws	
	Size		6g × 32 mm long, bugle head, self-drilling screws	
19.	Item na	me	Fast-fix washers and pin weld	
	Size		115 mm × 3 mm pins and 25 mm × 25 mm fast fix washers.	
Installa	ation met	hod		
two C-purlin se installed betwe framing (item 8 unexposed sid		two C-purlin se installed betwe framing (item 8 unexposed sid	me (item 4) was the main support for the test specimen, however, there were ections that acted as false slabs (200 mm tall). Steel stud framing (item 8) was een the C-purlins. PET insulation (item 11) was inserted within the steel 3) and was capped with 13 mm thick FR plasterboard (item 2) on the e and along the edges. The plasterboard was fixed with plasterboard screws x 300 mm centres on the periphery and 600 mm centres in-field.	
External wall:		The external section of the wall system largely consisted of an aluminium extrusion framing system (item 5), galvanised steel sheet backpan (item 3) and ACP cassette system (item 1). The external wall was screw fixed using angles. The ACP cassettes were 150 mm deep and were connected to the aluminium extrusion framing (item 5) using aluminium angles (item 6) and aluminium stiffeners (item 7). The angles (item 6) were screw fixed to the extrusions, the aluminium sheeting riveted to the angles, and the ACP cassettes riveted to the aluminium sheets. Sealant (item 13) was used to seal open ACP edges, screw fixings and rivet locations.		
framing (item insulation was combinations		framing (item s insulation was combinations (	item 3) was screw fixed and riveted to the back of the aluminium extrusion 5). Foil faced insulation (item 12) was installed within the external wall. The held to the steel backpan (item 3) with the aid of fast-fix washers and pin item 19) – at ~600 mm centres - that were welded to the backpan. There was between the backpan and the internal wall studwork.	

## 

## 3. Test procedure

Table 3 details the test procedure for this reaction to fire test.

#### Table 3 Test procedure

	procedure		
ltem	Detail		
Statement of compliance	The ad-hoc test – which was based off ISO 13785-1:2002 - was performed to determine the reaction to fire performance of an external wall cladding when exposed to heat from a simulated external fire with flames impinging directly upon a façade. The test utilises a burner used in ISO 13785-1:2002 with the specimen mimicking the as-is construction of the façade.		
Sampling / specimen selection	The laboratory was not involved in sampling or selecting the test specimen for the reaction to fire test. The results obtained during the test only apply to the test samples as received and tested by Warringtonfire.		
Test duration	Approximately 7 minutes		
Ambient	Start of the test	20 °C	
laboratory temperature	Minimum temperature	20 °C	
·	Maximum temperature	22 °C	
Instrumentation and equipment	<ul> <li>Eight mineral insulated metal sheathed (MIMS) Type K thermocouples with an overall diameter of 1.5 mm with the measuring junction insulated from the sheath were positioned 60 mm in front of the face of the test specimen. Refer to Figure 1 (TC011 – TC018) for details on positioning.</li> <li>Ten mineral insulated metal sheathed (MIMS) Type K thermocouples with an overall diameter of 1.5 mm with the measuring junction insulated from the sheath were positioned inside the specimen at the centre of the cavity. Refer to Figure 1 (TC001 – TC010) for details on positioning.</li> <li>The incident heat flux on the top of the specimen in line with the front face of test specimen was measured using one Schmidt-Boelter type heat flux gauge with a range of 0-50 kW/m<sup>2</sup>.</li> <li>The fire source was a propane (95% purity) gas burner 1.2 m long × 0.1 m deep × 0.15 m tall. The burner was placed on the floor below the specimen with approximately 10 mm overlap with the ACP.</li> </ul>		
Test procedure	<ul> <li>At least two minutes of baseline data was collected prior to burner ignition. Temperature and heat flux data was collected at 5 s intervals.</li> <li>The heat output from the burner was held at 200 kW for the duration of the test. The burner was then turned off and the specimen sprayed with water when excessive flaming was observed.</li> </ul>		
Test number	Test three of three.		
Variation between tests	The test was based off RTF230111 R2.0. The test specimens and burner output were the same, however, and test setup varied slightly. Test RTF230111 R1.0 allowed for flames to travel up the sides of the specimen as the burner was wider than the cassetted ACPs. In this test the exposure to the sides of the specimen was prevented. Plasterboard and mineral wool were used to direct the flames to the front of the specimen only from underneath.		

## 4. Test measurements and results

The results from the tests are summarised below. Photographs of the specimen are included in Appendix B.

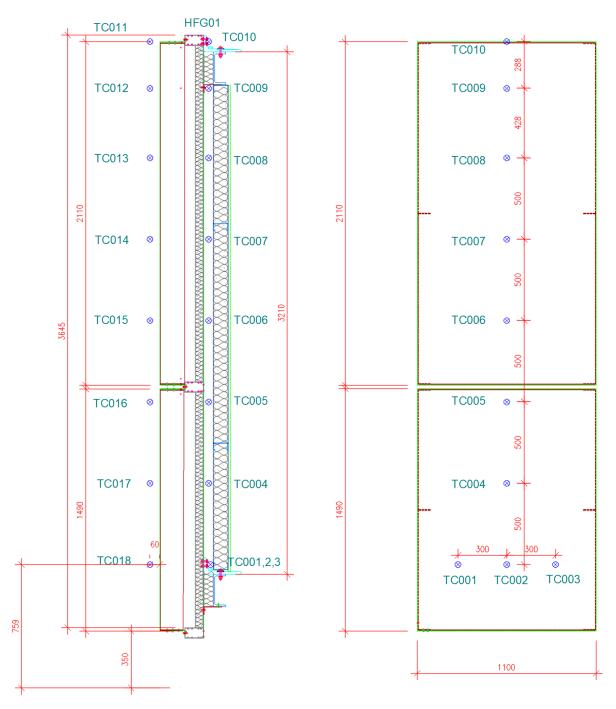


Figure 1 Instrumentation location



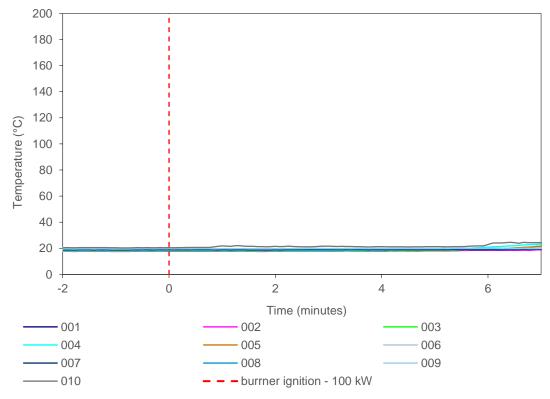


Figure 2 Internal temperature data collected by thermocouples placed within the cavity – between the internal and external segments of the specimen.

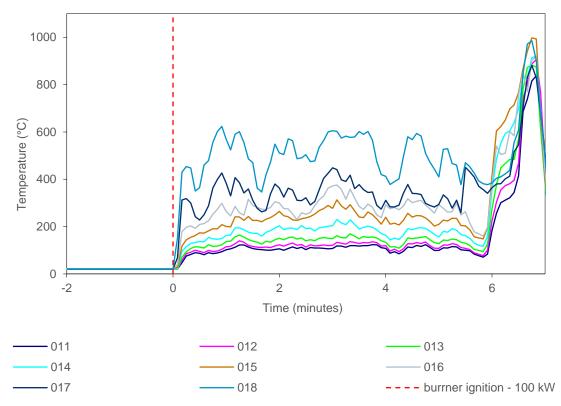


Figure 3 External temperature data collected by thermocouples placed 60 mm from the front face of the specimen.



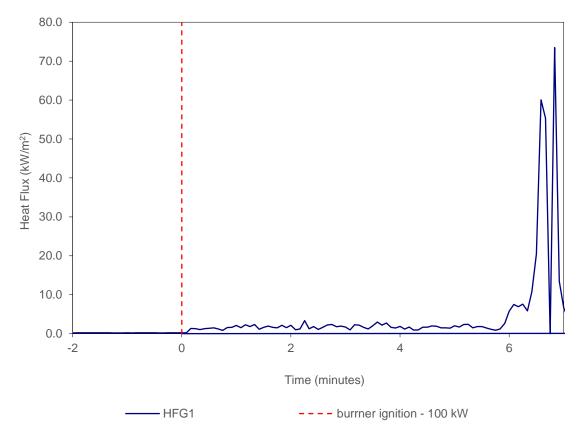


Figure 4 Heat flux data collected by heat flux gauges.

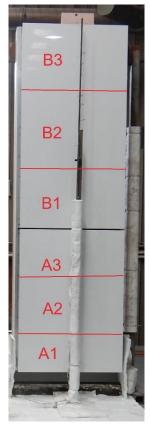


Figure 5 Designation for test specimen observations.



Table 4 shows the observations of any significant behaviour of the specimen during the test.

Video recordings were also taken of the test. A copy of the video recording is available upon request from the test sponsor or by contacting Cladding Safety Victoria. The video of the test should be viewed in conjunction the contents of this report.

		1001080			
Time Section		Section	Observation		
Min	Sec				
-2	00	All	Data collection started.		
0	00	All	The reaction to fire test was started with the burner ignited with a heat output set at 200 kW.		
0	06	А	Flames reached mid-height of the panel.		
0	19	A1	There was discolouration on the front face of the panel.		
0	36	A2	There was discolouration on the front face of the panel.		
1	37	B1	Flames reached the bottom of the panel.		
2	00	A1/A2	The panel started to deform.		
2	21	A3	There was discolouration on the front face of the panel.		
2	57	B1	There was discolouration on the front face of the panel.		
3	43	A1	There was flaming dripping debris from the bottom of the specimen.		
5	22	All of A	There was a large and sudden release of built-up gas causing flaming debris to shoot from the specimen.		
5	55	All of A	The flames have engulfed the lower panel. It is possible that the core is contributing to the fire.		
6	01	B3	Flames reached this section of the specimen.		
6	23	All	The panels have opened up and the core material is contributing to the fire.		
6	48	All	Flaming of the specimen was excessive. The power to the burner was cut and specimen was sprayed with water. The test ended.		

#### Table 4 Test observations

## 5. Application of test results

## 5.1 Test limitations

The results of these fire tests may be used to directly assess fire hazard, but it should be recognised that a single test method will not provide a full assessment of fire hazard under all fire conditions.

These results only relate to the behaviour of the specimen of the element of construction under the particular conditions of the test. They are not intended to be the sole criteria for assessing the potential fire performance of the element in use, and they do not necessarily reflect the actual behaviour in fires.

## 5.2 Variations from the tested specimen

This report details methods of construction, the test conditions and the results obtained when the specific element of construction described here was tested following the procedure outlined in Table 3. Any significant variation with respect to size, construction details, loads, stresses, edge or end conditions is not addressed by this report.

It is recommended that any proposed variation to the tested configuration should be referred to the test sponsor. They should then obtain appropriate documentary evidence of compliance from Warringtonfire or another accredited testing authority.

## 5.3 Uncertainty of measurements

Because of the nature of reaction to fire testing and the consequent difficulty in quantifying the uncertainty of measurements obtained from a reaction to fire test, it is not possible to provide a stated degree of accuracy of result.



## Appendix A Drawings of test assembly

The drawings of the test assembly in Figure 6 to Figure 9 were provided representatives of Warringtonfire. Dimensions, unless specified, are in mm.

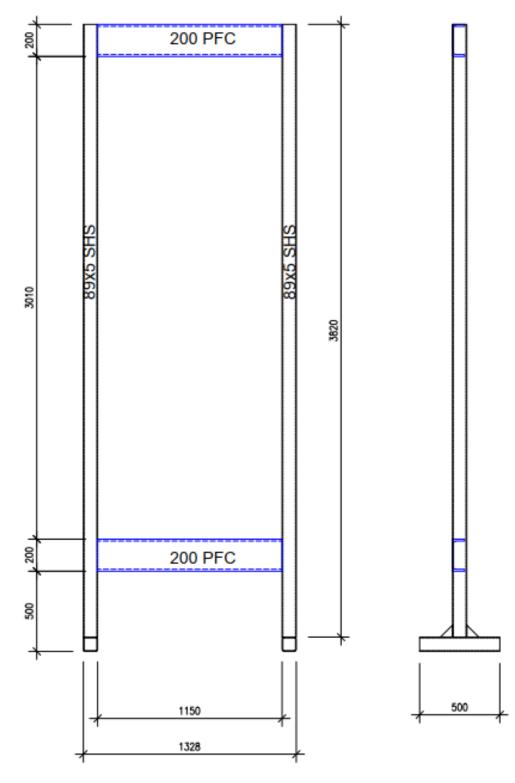


Figure 6 Elevation of rig support.



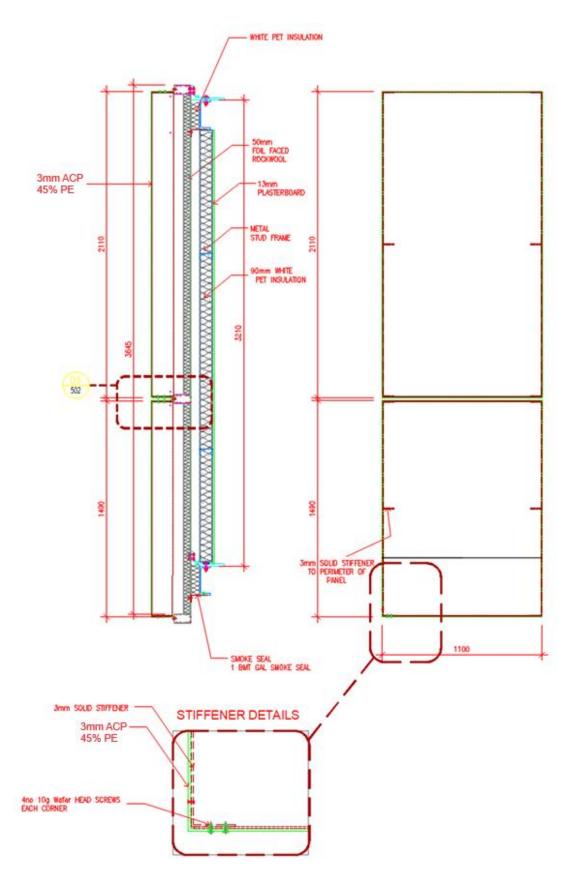


Figure 7 System assembly – Front and side view



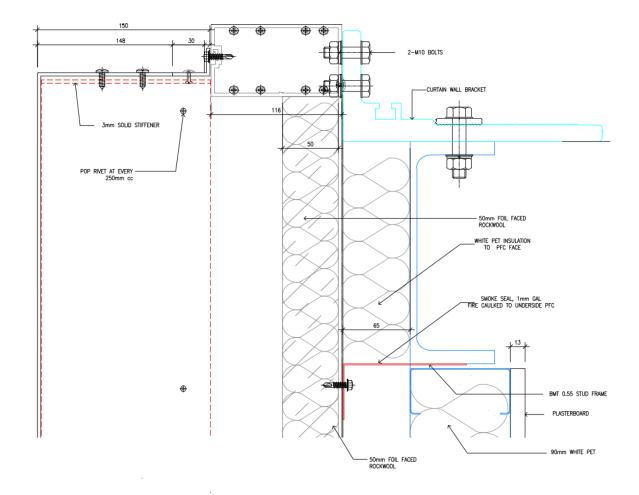


Figure 8 System assembly – top edge detail

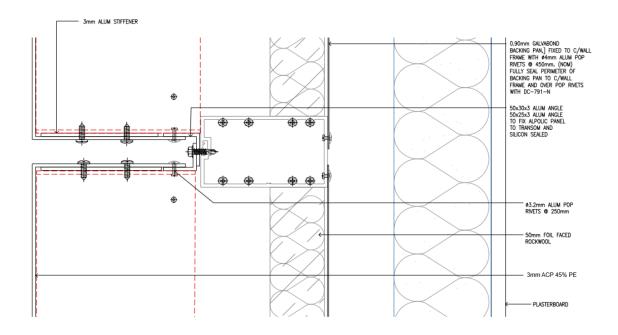


Figure 9 System assembly – middle join detail (D05)



## Appendix B Photographs



Figure 10 The specimen before the reaction to fire test





Figure 11 The specimen before the reaction to fire test – unexposed side





Figure 12 The specimen 1 minute into the test (burner output at 200 kW)





Figure 13 The specimen 2 minutes into the test (burner output at 200 kW)





Figure 14 The specimen 3 minutes into the test (burner output at 200 kW)





Figure 15 The specimen 4 minutes into the test (burner output at 200 kW)





Figure 16 The specimen 5 minutes into the test (burner output at 200 kW)





Figure 17 The specimen 6 minutes into the test (burner output at 200 kW)





Figure 18 The specimen 6 minutes 17 seconds into the test (burner output at 200 kW)





Figure 19 The specimen 6 minutes 22 seconds into the test (burner output at 200 kW)





Figure 20 The specimen 6 minutes 37 seconds into the test (burner output at 200 kW)





Figure 21 The specimen 6 minutes 46 seconds into the test (burner output at 200 kW) – 2 seconds before end of test.

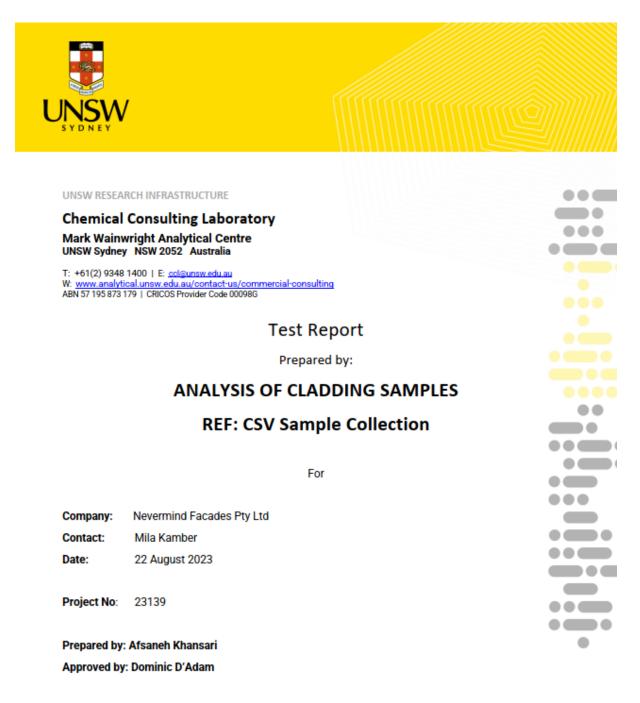




Figure 22 The specimen after the test



## Appendix C Chemical analysis results



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## Analysis of Cladding Samples, CSV Sample Collection

#### 1. SAMPLES

One box containing five ACP cores was received for analysis. The samples were identified as follows:

CCL sample coding	Client sample coding
23139-1	CSV #02
23139-2	CSV #03
23139-3	CSV #04
23139-4	CSV #08
23139-5	CSV #09

CCL has been asked to identify the polymer and the filler (s) in the sample by FT/IR, quantitate and identify the mineral filler in the sample and classify them in accordance with the ICA cladding scheme.

#### 2. METHODOLOGY AND RESULTS

The aluminium metals were removed from the ACPs cladding polymers, and the flat surface of the polymer samples was abraded to remove any surface adhesive. The surface of each sample was analysed directly by FTIR. The FT-IR spectra are presented in Figures 1-5.

The core of each sample was then ashed to determine its percentage mineral content (Table 1). If sufficient (>0.5 g) ash had been produced it would have been analysed for elemental composition by X ray fluorescence spectroscopy. Results are presented in Table 2.

Table 1 Ash content of 23139-1 to 23139-5

Sample coding	Ash content (w/w%)
23139-1	19.1
23139-2	21.9
23139-3	31.9
23139-4	38.3
23139-5	18.9

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Element Oxide wt.%	23139-3	23139-4
Na <sub>2</sub> O	0.46	0.50
MgO	4.59	6.80
Al <sub>2</sub> O <sub>3</sub>	1.08	0.96
SiO <sub>2</sub>	7.09	6.63
P <sub>2</sub> O <sub>5</sub>	0.06	0.07
SO <sub>3</sub>	1.43	2.71
K <sub>2</sub> O	0.17	0.16
CaO	70.53	59.61
TiO <sub>2</sub>	1.17	1.80
V <sub>2</sub> O <sub>5</sub>	<0.01	0.01
Cr <sub>2</sub> O <sub>3</sub>	<0.01	<0.01
Mn <sub>3</sub> O <sub>4</sub>	<0.01	<0.01
Fe <sub>2</sub> O <sub>3</sub>	0.90	0.90
NiO	<0.01	<0.01
CuO	0.14	0.10
ZnO	2.48	2.47
SrO	0.10	0.17
ZrO <sub>2</sub>	<0.01	<0.01
BaO	3.02	6.15
HfO₂	<0.01	<0.01
PbO	<0.01	<0.01
L.O.I.	ND	ND

Table 2 Elemental composition of 23139-3 (CSV-04) and 23139-4 (CSV-08)

NOTE: (i) L.O.I.= loss on ignition at 1,050 °C. (ii) ND = not determined



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#### 2. CONCLUSIONS

The cladding CSV #02 consisted of 80.9% poly(ethylene-vinyl acetate) (PEVA) polymer and 19.1% other inert material.

#### The cladding sample #1, CSV #02 is classified as ICA category A.

The cladding CSV #03 consisted of 78.1% poly(ethylene-vinyl acetate) (PEVA) polymer and 21.9% other inert material.

The cladding sample #2, CSV #03 is classified as ICA category A.

The cladding CSV #04 consisted of 2.1% magnesium hydroxide, 40.2% calcium carbonate, 7.9% other inert material and approximately 49.8% poly(ethylene-vinyl acetate) (PEVA) polymer.

The cladding sample 3, CSV #04 is classified as ICA category A.

The cladding CSV #08 consisted of 3.8% magnesium hydroxide, 40.7% calcium carbonate, 12.9% other inert material and approximately 42.6% poly(ethylene-vinyl acetate) (PEVA) polymer.

#### The cladding sample 4, CSV #08 is classified as ICA category A.

The cladding CSV #09 consisted of 81.1% poly(ethylene-vinyl acetate) (PEVA) polymer and 18.9% other inert material.

The cladding sample 5, CSV #09 is classified as ICA category A.

#### The ICA Classification assigned is correct as per the September 2020 revision of the ICA Guidelines.

The calculation for magnesium hydroxide content assumes that all magnesium found is present as the hydroxide. The calculation for calcium carbonate content assumes that all calcium found is present as calcium carbonate.

The reader is reminded that we can only analyse and classify the content of samples actually presented to us. We can offer no guarantee that this composition or classification is valid for cladding as a whole, because some types of cladding can be inhomogeneous, and a sample may not be representative of the cladding as a whole. Anyone using our results should consider these sampling issues and uncertainties before they generalise the results we present to anybody of cladding as a whole.



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Afsaneh Khansari (PhD) Technical Officer Chemical Consulting Laboratory Mark Wainwright Analytical Centre, UNSW 22 August 2023

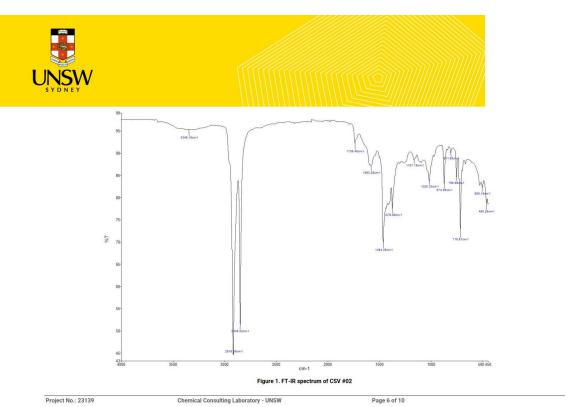


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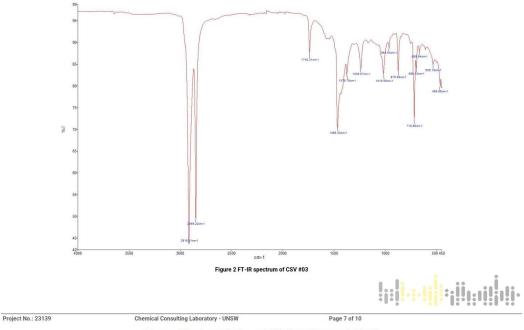
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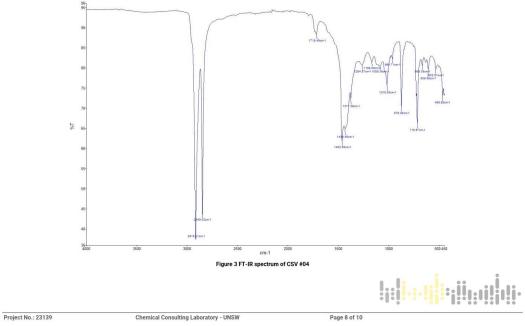


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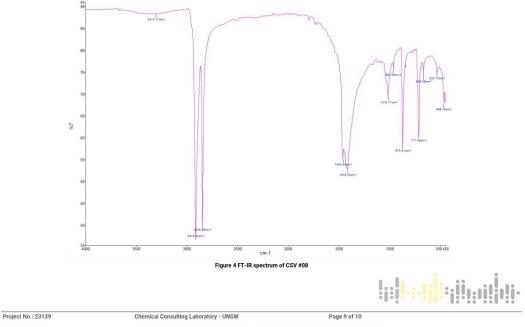


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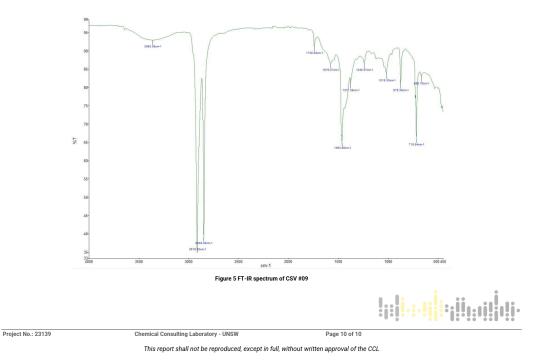


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# **Global locations**



Warringtonfire Australia Pty Ltd ABN 81 050 241 524

#### Perth

Suite 4.01, 256 Adelaide Terrace Perth WA 6000 Australia T: +61 8 9382 3844

#### Sydney

Suite 802, Level 8, 383 Kent Street Sydney NSW 2000 Australia T: +61 2 9211 4333

#### General conditions of use

Canberra

Unit 10, 71 Leichhardt Street Kingston ACT 2604 Australia T: +61 2 6260 8488

#### Brisbane

Suite B, Level 6, 133 Mary Street Brisbane Qld 4000 Australia T: +61 7 3238 1700

#### Melbourne

Level 4, 152 Elizabeth Street Melbourne Vic 3000 Australia T: +61 3 9767 1000

Melbourne - NATA accredited laboratory

409-411 Hammond Road Dandenong South Vic 3175 Australia T: +61 3 9767 1000

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