



Reaction to fire test report

Test standard: Ad-hoc test based off ISO 13785-1:2002

Test sponsor: Cladding Safety Victoria (CSV)

System: Aluminium composite panel (ACP) and glazing external wall cladding system

Job number: RTF230148

Test date: 14 February 2024 Revision: R3.0



Quality management

Revision	Date	Information a	bout the report		
R3.0	28 March 2024	Description	Initial issue.		
			Prepared by	Reviewed by	Authorised by
		Name			
		Signature			
				1	

Warringtonfire* Australia Pty Ltd ABN 81 050 241 524

Test standard: General accordance with ISO 13785-1:2002

Job number: RTF230148

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1. Introduction

This report documents the findings of test three of three ad-hoc reaction to fire tests for an Aluminium composite panel (ACP) and glazing external wall cladding system performed on 14 February 2024. The test was based off some general requirements of ISO 13785-1:2002.

Warringtonfire performed the test at the request of the test sponsor listed in Table 1.

Table 1 Test sponsor details

Test sponsor	Address
Cladding Safety Victoria (CSV)	717 Bourke Street Docklands, VIC 3808
	Australia

2. Test specimen

2.1 Schedule of components

Table 2 describes the test specimen and lists the schedule of components. These were provided by the representatives of the test sponsor and surveyed by Warringtonfire. All measurements were done by Warringtonfire – unless indicated otherwise.

Detailed drawings of the test specimen are provided in Appendix A.

Table 2 Schedule of components

Item	Description				
Clado	Cladding				
1.	Item name FR aluminium composite panel (ACP) panel				
	Product	FR Aluminium Composite Panel - 4 mm Dark Oak/Matte White			
	Manufacturer/supplier				
	Material	The material was nominated as panels consisting of two layers of aluminium sheets sandwiching a layer (core) with 45 % polyethylene (PE) and inorganic filler. Analysis conducted by the analytical centre of UNSW showed that the core consisted of polyethylene-vinyl acetate (PEVA) - found to be 43.9 % w/w - whilst the remainder of the material was found to be 45.3 % magnesium hydroxide, 6.1 % calcium carbonate and 4.8 % other inert material. Refer to Appendix C for more detailed results.			
	Size	Total panel thickness – 4.0 mm Core thickness – 2.9 mm Skin thickness – 0.5 mm (both) Refer to Appendix A for individual panel sizing details.			
	Areal density	Full panel – 6.9 kg/m² (measured)			
	Colour	Skins Front skin – Dark brown oak pattern Back skin – Matte white			
		Core Light grey			
	Marking (representative panel)				
2.	Item name	Back-pan			
	Product	Nominally 0.9 mm thick Galvabond sheet measured 0.6 mm			
	Supplier				

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Item	Description			
	Material	Galvanised steel		
	Batch	Unknown		
	Size	1160 mm wide × 3700 mm tall, 0.6 mm thick – in segments.		
Glazi	ng			
3.	Item name	Double glazing		
	Material	6 mm Clear Heat Strengthened\12B (Argon filled cavity) \6.5 HU		
	Size (nominal)	1188 mm wide × 1800 mm tall × 6 mm/12 mm/6.5 mm with a 12 mm black spacer.		
	Manufacturer/Supplier			
	Batch			
4.	Item name	Single glazing		
	Material	6 mm Clear Heat Strengthened		
	Size (nominal)	1182 mm wide × 1800 mm tall × 6 mm thick		
	Manufacturer/Supplier			
	Batch			
Fram	ing			
5.	Item name	Test rig frame - 90 × 90 SHS and 200 × 90 PFC frame		
	Material	Painted steel		
	Size	90 mm × 90 mm × 5 mm thick and 200 mm × 90 mm × 10 mm thick – refer to Figure 12.		
6.	Item name	Aluminium curtain wall transom/mullions (rectangular hollow sections) – framing		
	Material	Aluminium		
	Size	65 mm to 70 mm wide × 116 mm deep × 3 mm thick.		
	Manufacturer/Supplier			
7.	Item name	Aluminium angles - framing		
	Size	25 mm wide × 50 mm deep × 3 mm thick		
	Material	Aluminium		
	Manufacturer/Supplier			
8.	Item name	Aluminium angles – for middle double back-pan unit.		
	Size	25 mm wide × 50 mm deep × 3 mm thick		
	Material	Aluminium		
	Manufacturer/Supplier			
	Installation	Used to secure the secondary back-pan in the within the middle module. The angle was screw fixed to both the back-pan (item 2) and the aluminium framing (item 6) using screws (item 18).		
9. Item name Aluminium stiffener - framing		Aluminium stiffener - framing		
	Size	3 mm thick × 150 mm deep		
	Material	Aluminium		
	Manufacturer/Supplier			



Item	Description			
10.	Item name	Curtain wall bracket		
	Size	150 mm deep (7 mm thick) × 75 tall (10 mm thick) × 100 mm wide		
	Installation	Used to secure the 3 modules to the test rig using tek screws.		
Smok	re seal	Caraca and		
11.	Item name	Smoke seal		
	Size	0.55 mm thick galvanised steel		
	Manufacturer/Supplier			
Penet	tration			
12.	Item name	Exhaust		
	Size	Backing plates: 355 mm × 355 mm × 0.6 mm thick Large tube: Ø150 mm × 600 mm long × 0.5 mm thick Cap: Ø240 mm × 85 mm deep × 0.6 mm thick Connecting strips: 45 mm × 5 mm wide × 0.5 mm thick		
	Material	Galvanised steel		
	Manufacturer/Supplier			
	Pictures	Exposed side Unexposed side		
	Installation	The penetrating element was a galvanised steel tube. On the glazing side was a circular weather cowl. Between the glazing and the inner back-pan was a square compartment made from galvanised steel which hid the tubing.		
Insula	ation			
13.	Item name	90 mm thick polyethylene terephthalate (PET) insulation		
	Density	10 kg/m³		
	Manufacturer/Supplier			
14.	Item name	50 mm thick aluminium - with fibre-glass mesh - foil faced rockwool insulation		
	Density of core	40 kg/m ³		
	Manufacturer/Supplier			
Seala	int/Adhesive			
15.	Item name	Weathering sealant - silicone sealant		
	Product name			
	Manufacturer/Supplier			
	Usage	Placed at ACP edges and screw and rivet locations.		
16.	Item name	Back-pan sealant - Fire-rated mastic		
	Product name			
	Manufacturer/Supplier			



Item	Description		
	Usage	Used between the back-pans (item 2) and the aluminium framing (item 7).	
17.	Item name	Penetration sealant	
	Product name		
	Manufacturer/Su	pplier Parameter	
	Usage	Used between the back-pans (item 2) and the aluminium framing (item 7).	
Fixin	gs		
18.	Item name	Tek screws SDS – zinc coated steel – for fixing the back-pan	
	Size	10g × 24 mm long	
	Installation	Used to fix aluminium angles (item 8) to the aluminium frame (item 6) at max. 500 mm centres	
19.	Item name	Wafer head screws – zinc coated steel	
	Size	10g × 16 mm long	
	Installation	Used to fix aluminium angles (item 8) to the aluminium frame (item 6) at max. 500 mm centres	
20.	Item name	Wafer head screws – zinc coated steel	
	Size	10g × 20 mm long	
	Installation	Used to fix the penetration backing plate (item 12) to the back-pan (item 2) of the central module.	
21.	Item name	Wafer head screws – zinc coated steel	
	Size	10g × 21 mm long	
	Installation	Used to fix ACP (item 1) to the aluminium stiffener (item 9) – four per corner.	
22.	Item name	Aluminium rivets	
	Size	Ø4 mm	
23.	Item name	Fast-fix washers and pin weld (to hold insulation)	
	Size	115 mm × 3 mm pins and 25 mm × 25 mm fast fix washers.	
24.	Item name	Tek screws for curtain wall bracket	
	Size	14 g × 35 mm long	
25.	Item name	Tek screws for smoke seal to false slab i.e. C-Purlin	
	Size	14 g × 35 mm long	
Insta	llation method		
Test r	w 3 te	ne test rig frame (item 5) was the main support for the test specimen, however, there ere two C-purlin sections that acted as false slabs (200 mm tall). The test specimen, off modules – interconnected through aluminium framing (item 6), was fixed to the st rig using curtain wall brackets (item 10) and fixings (item 24) – see Figure 14 & gure 16. Each module extended from the bottom of the specimen to the top.	
Frami	W Si	ne main framing for the external wall was composed of aluminium extrusions (item 6) hich were screw fixed together. Aluminium angles (item 8) – horizontal edges - and iffeners (item 9) – on the vertical edges - were fixed to the aluminium framing (item 6), sing wafer head screws (item 20) and aluminium rivets (item 22), respectively.	



Α.	lensen	Hughe	es Com	pany

Item Description	
Cladding:	The front face of the specimen was cladded with cassetted ACPs (item 1), which were fixed to the aluminium stiffeners (item 9) and the aluminium angles (item 8) using aluminium rivets (item 22), 2-off at 300 mm centres. See Figure 13 for panel locations.
	The back side of the framing was closed off with steel back-pans (item 2) screw fixed (item 18) at 300 mm centres. PET insulation (item 13) was fixed to the back-pan using fast-fix washers and pin combinations (item 19) that were welded to the back-pan. The centre module had an extra back-pan behind the glazing (item 4). This was fixed to the aluminium framing (item 6) using screws (item 18) and aluminium angles (item 8). Foil-faced rockwool insulation (item 14) was inserted between the two back-pans (item 2) of the centre module.
Glazing The glazing, both double (item 3) and single (item 4), were attached to t framing (item 6) as shown in Figure 13 to Figure 23 and Figure 26. The sealed around the perimeter with weather sealant (item 15).	
Smoke seal	Smoke seal barrier (item 11) was attached to C-purlins of the test rig (item 5) with screw fixings (item 24) at approximate 600 mm centres. PET insulation (item 13) was installed into the 60 mm wide cavity above the barrier (item 12).
Penetration	The penetration went through holes in the single glazing (item 4) and back-pans (item 2) of the second module. These were fixed to the back-pan and the window with a steel sheet (backing plate), using screws and sealant and just sealant, respectively.



Test procedure 3.

Table 3 details the test procedure for this reaction to fire test.

Table 3 **Test procedure**

Statement of compliance The ad-hoc test – which was based off ISO 13785-1:2002 - was performed to determine the reaction to fire performance of an external wall cladding when exposed to heat from a simulated external fire with flames impinging directly upor a façade. The test utilises a burner used in ISO 13785-1:2002. Sampling / specimen selection The laboratory was not involved in sampling or selecting the test specimen for the reaction to fire test. The results obtained during the test only apply to the test samples as received and tested by Warringtonfire. Test duration 60 minutes 21 mineral insulated metal sheathed (MIMS) Type K thermocouples with an overall cliameter of 1.5 mm with the measuring junction insulated from the sheath were positioned 60 mm in front of the outer ACP face of the test specimen. Refer to Figure 1 for details on positioning. The incident heat flux on the top of the specimen in line with the front face of test specimen was measured using a Schmidt-Boelter type heat flux gauges with a range of 0-20 kW/m². The incident heat flux 500 mm behind the outer glazing's – burner side and non-burner side – was measured using two Schmidt-Boelter type heat flux gauges with a range of 0-20 kW/m². The incident heat flux 80 mm behind the central glazing was measured using a Schmidt-Boelter type heat flux gauges with a range of 0-20 kW/m². Temperatures above and below the cladding were measured by seven 100 mm × 100 mm × 0.7 mm plate thermocouples with mineral insulated metal sheathed (MIMS) Type K thermocouples with an overall diameter of 1 mm with the measuring junction electrically insulated from the sheath. The thermocouple hot junction was fixed to the geometric centre of the plate by a small steel strip made from the same material as the plate. The plate thermocouples included 97 mm × 97 mm × 10 mm inorganic insulation pads. Before the first use of the plate thermocouples, they were aged by being exposed to heat in a fire-resistance test furnace for 90 min under the standard tempera		
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specimen was measured using a Schmidt-Boelter type heat flux gauge with a range of 0-20 kW/m². The incident heat flux 500 mm behind the outer glazing's – burner side and non-burner side – was measured using two Schmidt-Boelter type heat flux gauges with a range of 0-20 kW/m². The incident heat flux 80 mm behind the central glazing was measured using a Schmidt-Boelter type heat flux gauge with a range of 0-20 kW/m². Temperatures above and below the cladding were measured by seven 100 mm × 100 mm × 0.7 mm plate thermocouples with mineral insulated metal sheathed (MIMS) Type K thermocouples with an overall dameter of 1 mm with the measuring junction electrically insulated from the sheath. The thermocouple hot junction was fixed to the geometric centre of the plate by a small steel strip made from the same material as the plate. The plate thermocouples included 97 mm × 97 mm × 10 mm inorganic insulation pads. Before the first use of the plate thermocouples, they were aged by being exposed to heat in a fire-resistance test furnace for 90 min under the standard temperature/ time curve Refer to Figure 1 for details on positioning. The fire source was a propane (95% purity) gas burner 1.2 m long × 0.1 m deep to 0.15 m tall. The burner was placed on the floor below the specimen with approximately 15 mm overlap with the ACP. Test procedure At least two minutes of baseline data was collected prior to burner ignition. Temperature and heat flux data was collected at 5 s intervals. The heat output from the burner was held at 300 kW for the 30 minutes. The burner was then turned off and data recorded for the next 30 minutes.	Instrumentation and equipment	overall diameter of 1.5 mm with the measuring junction insulated from the sheath were positioned 60 mm in front of the outer ACP face of the test
burner side – was measured using two Schmidt-Boelter type heat flux gauges with a range of 0-20 kW/m². The incident heat flux 80 mm behind the central glazing was measured using a Schmidt-Boelter type heat flux gauge with a range of 0-20 kW/m². Temperatures above and below the cladding were measured by seven 100 mm × 100 mm × 0.7 mm plate thermocouples with mineral insulated metal sheathed (MIMS) Type K thermocouples with an overall diameter of 1 mm with the measuring junction electrically insulated from the sheath. The thermocouple hot junction was fixed to the geometric centre of the plate by a small steel strip made from the same material as the plate. The plate thermocouples included 97 mm × 97 mm × 10 mm inorganic insulation pads. Before the first use of the plate thermocouples, they were aged by being exposed to heat in a fire-resistance test furnace for 90 min under the standard temperature/ time curve Refer to Figure 1 for details on positioning. The fire source was a propane (95% purity) gas burner 1.2 m long × 0.1 m deep 0.15 m tall. The burner was placed on the floor below the specimen with approximately 15 mm overlap with the ACP. Test procedure At least two minutes of baseline data was collected prior to burner ignition. Temperature and heat flux data was collected at 5 s intervals. The heat output from the burner was held at 300 kW for the 30 minutes. The burner was then turned off and data recorded for the next 30 minutes.		The incident heat flux on the top of the specimen in line with the front face of test specimen was measured using a Schmidt-Boelter type heat flux gauge with a range of 0-20 kW/m ² .
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100 mm × 0.7 mm plate thermocouples with mineral insulated metal sheathed (MIMS) Type K thermocouples with an overall diameter of 1 mm with the measuring junction electrically insulated from the sheath. The thermocouple hot junction was fixed to the geometric centre of the plate by a small steel strip made from the same material as the plate. The plate thermocouples included 97 mm × 97 mm × 10 mm inorganic insulation pads. Before the first use of the plate thermocouples, they were aged by being exposed to heat in a fire-resistance test furnace for 90 min under the standard temperature/ time curve Refer to Figure 1 for details on positioning. The fire source was a propane (95% purity) gas burner 1.2 m long × 0.1 m deep = 0.15 m tall. The burner was placed on the floor below the specimen with approximately 15 mm overlap with the ACP. Test procedure At least two minutes of baseline data was collected prior to burner ignition. Temperature and heat flux data was collected at 5 s intervals. The heat output from the burner was held at 300 kW for the 30 minutes. The burner was then turned off and data recorded for the next 30 minutes. Test number Test three of three.		
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Temperature and heat flux data was collected at 5 s intervals. The heat output from the burner was held at 300 kW for the 30 minutes. The burner was then turned off and data recorded for the next 30 minutes. Test number Test three of three.		
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		'
Variation to test one The laboratory conditions during the tests may vary.	Test number	Test three of three.
	Variation to test one	The laboratory conditions during the tests may vary.

Test standard: General accordance with ISO 13785-1:2002

Job number: RTF230148
Test sponsor: Cladding Safety Victoria (CSV)



4. Test measurements and results

The results from the tests are summarized below. Photographs of the specimen are included in Appendix B.



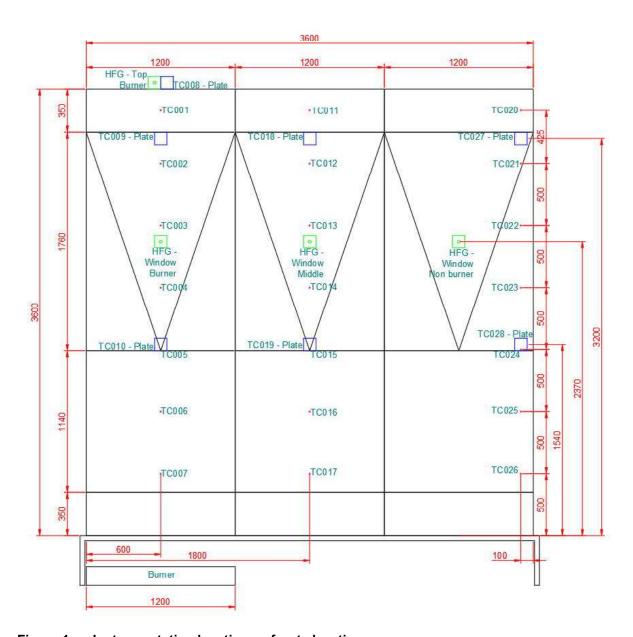


Figure 1 Instrumentation locations – front elevation

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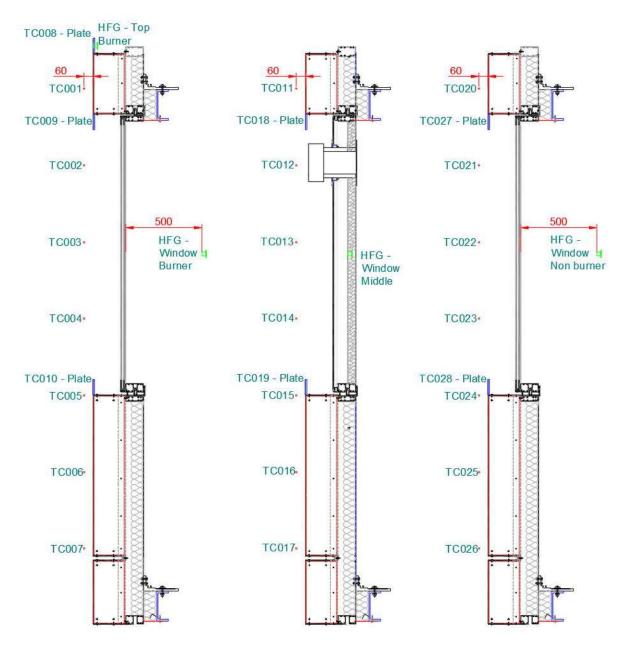


Figure 2 Instrumentation locations – sections



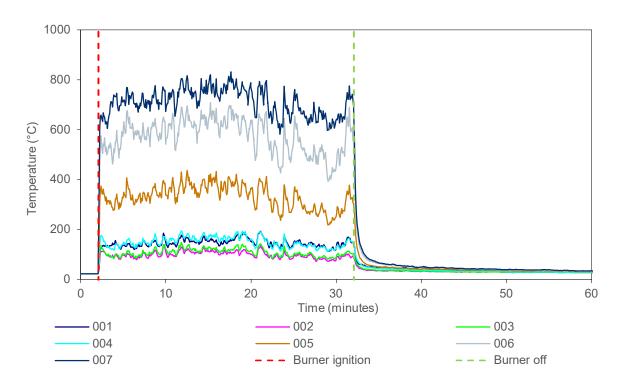
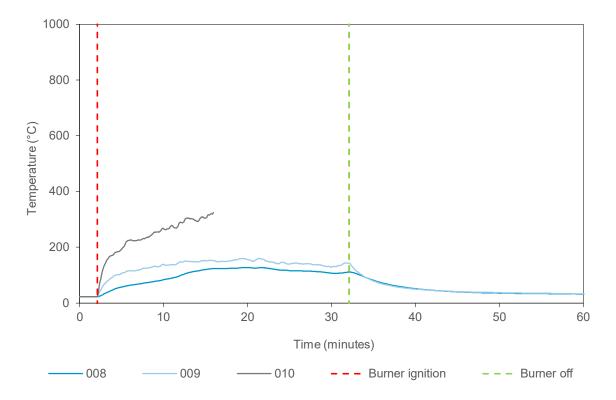


Figure 3 External temperature data collected by thermocouples placed 60 mm from the front face of the specimen - in-line with the burner



External temperature data collected by plate thermocouples in-line with ACP, Figure 4 above and below, respectively - in-line with the burner¹

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¹ Thermocouple 010 malfunctioned during the test, thus data after malfunction was removed.

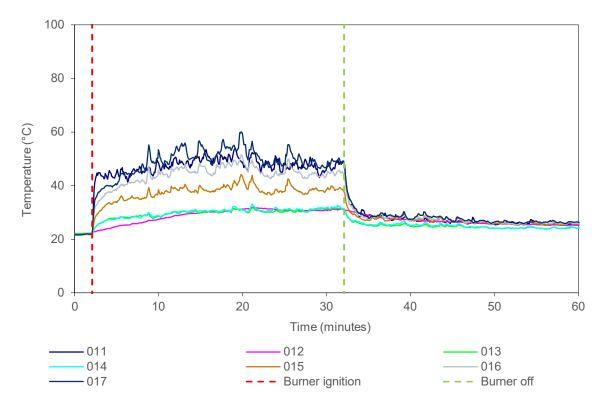
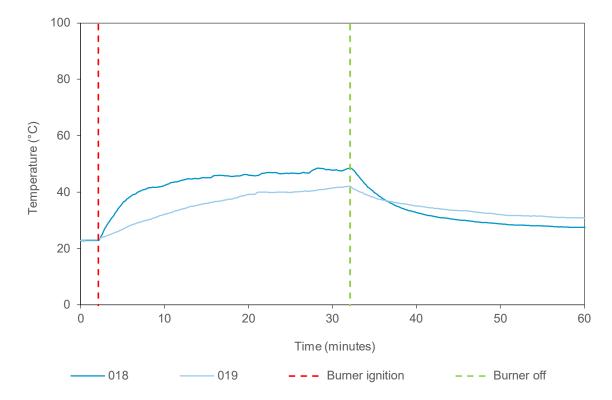


Figure 5 External temperature data collected by thermocouples placed 60 mm from the front face of the specimen - central module



External temperature data collected by thermocouples in-line with ACP, above Figure 6 and below, respectively - central module

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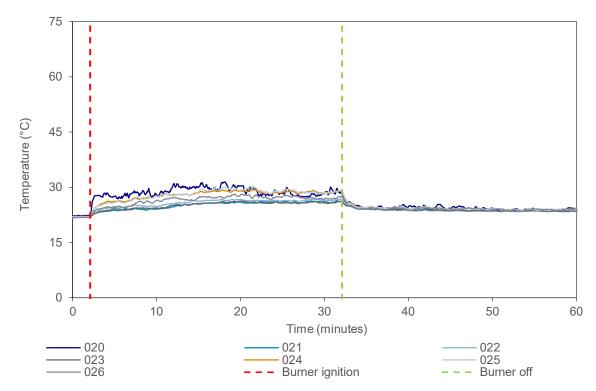


Figure 7 External temperature data collected by thermocouples placed 60 mm from the front face of the specimen – away from burner

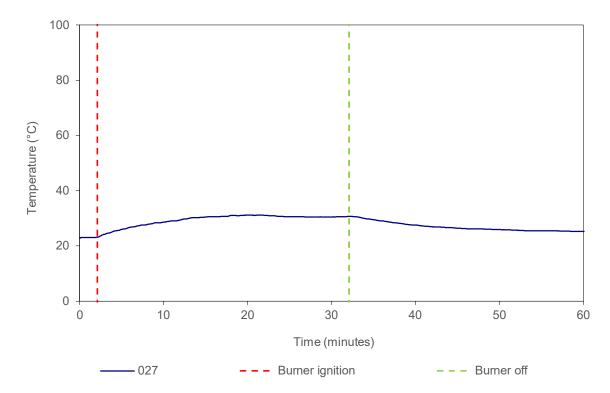


Figure 8 External temperature data collected by thermocouples in-line with ACP, above and below, respectively – away from burner²

² Thermocouple 028 malfunctioned during the test, thus causing spikes during the data collection process.



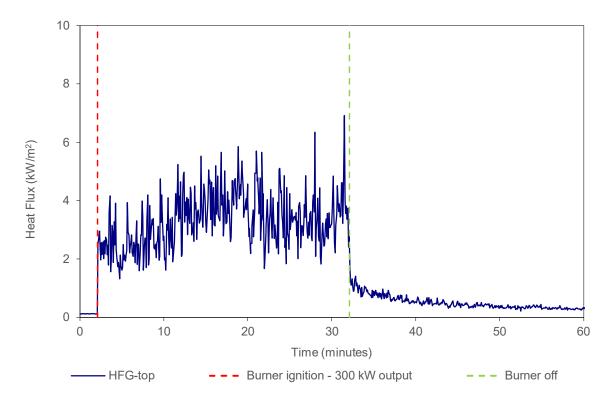


Figure 9 Heat flux data collected by heat flux gauge at the top of the specimen above the burner

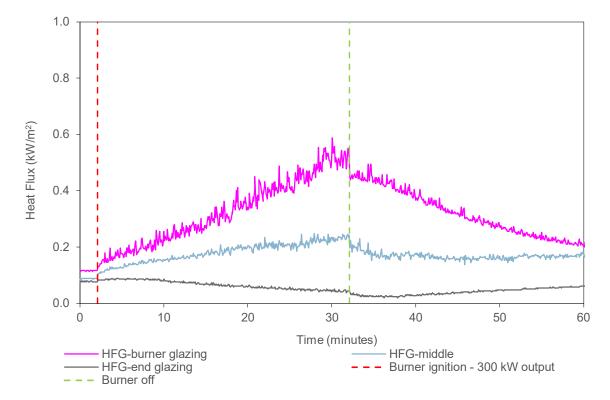


Figure 10 Heat flux measured by heat flux gauges behind the glazing units





Designation of section for the test observations Figure 11



Table 4 shows the observations of any significant behaviour of the specimen during the test. Figure 11 shows the panel and glazing designations sighted in the observations.

Video recordings were also taken of the test from approximately 4 metres in front of the specimen and from 2 metres on a 45 $^\circ$ angle behind the specimen.

Table 4 Test observations

	Sec	System	Observation	
	Sec			
-2				
	00	-	Data collection started.	
0	00	-	The reaction to fire test was started with the burner ignited with a heat output set at 300 kW.	
1	30	A1/A2	The paint of the front face of the panel started to flake off.	
2	00	A3	The flames had reached to the glazing face.	
3	38	Α	Smoke started to escape from the unexposed side of the specimen.	
4	00	Α	A pop sound was heard from the specimen.	
4	46	A3	Smoke started to escape from the bottom edge of the glazing.	
5	32	A/B	Smoke started to escape from the joint between the modules.	
6	58	B1/B2	Smoke started to escape from the horizontal joint between the panels.	
9	37	A1/A2	Flames started to spread along the horizontal joint between the panels.	
17	06	A4	The panel face started to deform slightly.	
18	25	A1	The bottom of the panel face started to open up.	
24	30	A1	A build up of gas was released from the panel.	
26	35	A2	The panel face was visibly opened up.	
27	37	A3	The bottom edge of the glazing was flaming independently.	
28	47	A3	The lower east edge of the glazing was flaming independently.	
30	00	-	The burner was turned off.	
30	05	Α	Panel A1 and A2 was still flaming. Lower east corner of glazing in A3 is still flaming.	
33	23	A3	The east edge flames had spread upwards, halfway up the glazing.	
35	25	A1/A2	The sustained flaming of the panel had died, leaving intermittent flaming. The panels were still smoking.	
38	00	A3	The glazing was visibly curved outwards.	
40	57	A3	The flames on the vertical east edge has gotten to the top, with the flames at the bottom dying out.	
42	35	A3	All glazing fire had died off.	
48	27	А	All smoking from the top of the specimen had died off.	
57	20	A2	The smoke from the panel had stopped.	
60	00	-	The test was ended.	

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5. **Application of test results**

5.1 **Test limitations**

The results of these fire tests may be used to directly assess fire hazard, but it should be recognised that a single test method will not provide a full assessment of fire hazard under all fire conditions.

These results only relate to the behaviour of the specimen of the element of construction under the particular conditions of the test. They are not intended to be the sole criteria for assessing the potential fire performance of the element in use, and they do not necessarily reflect the actual behaviour in fires.

5.2 Variations from the tested specimen

This report details methods of construction, the test conditions and the results obtained when the specific element of construction described here was tested following the procedure outlined in Table 3. Any significant variation with respect to size, construction details, loads, stresses, edge or end conditions is not addressed by this report.

It is recommended that any proposed variation to the tested configuration should be referred to the test sponsor. They should then obtain appropriate documentary evidence of compliance from Warringtonfire or another accredited testing authority.

5.3 **Uncertainty of measurements**

Because of the nature of reaction to fire testing and the consequent difficulty in quantifying the uncertainty of measurements obtained from a reaction to fire test, it is not possible to provide a stated degree of accuracy of result.

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Appendix A Drawings of test assembly

The drawings of the test assembly in Figure 12 to Figure 26 were provided by the representatives of Warringtonfire. Dimensions, unless specified, are in mm.

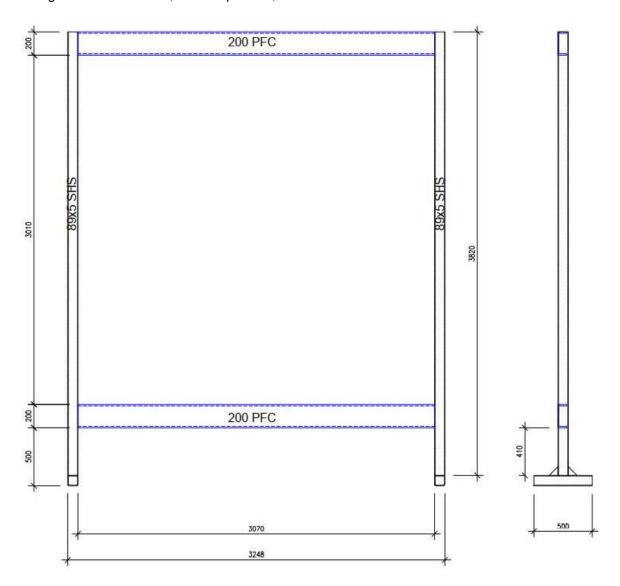


Figure 12 Elevation of rig support

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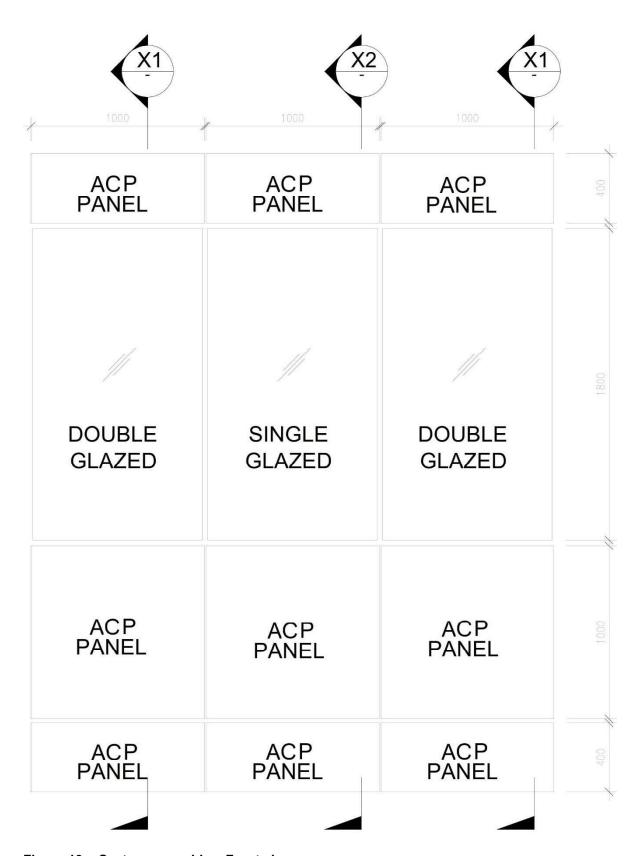


Figure 13 System assembly - Front view

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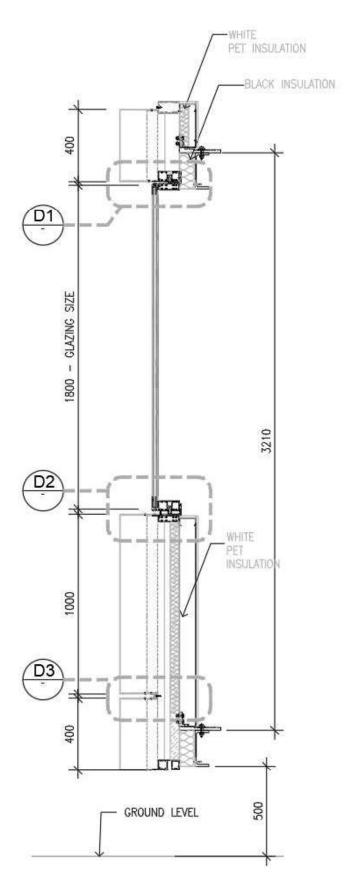


Figure 14 System assembly – vertical cross-sectional view X1

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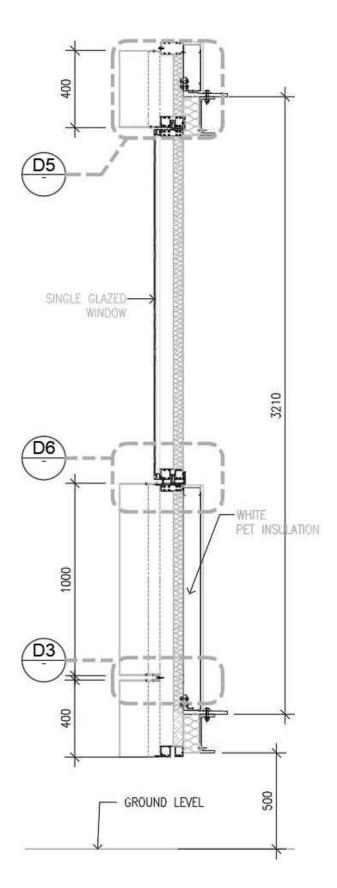


Figure 15 System assembly – vertical cross-sectional view X2

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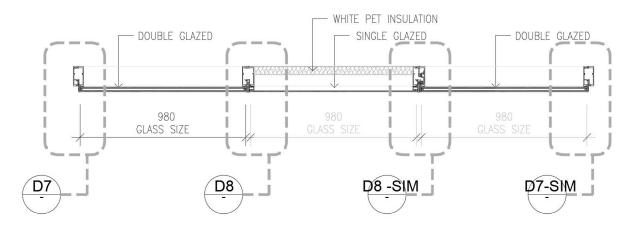


Figure 16 System assembly – horizontal mid height cross-sectional view

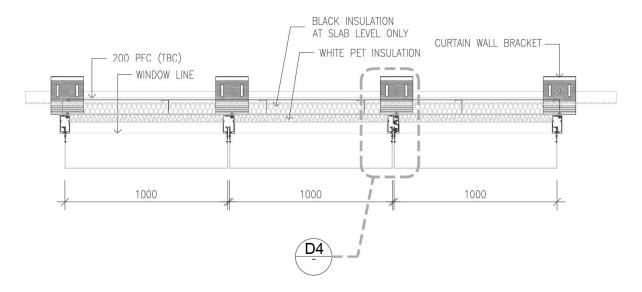


Figure 17 System assembly -top view

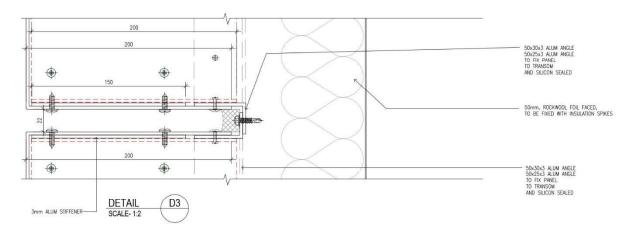


Figure 18 System assembly – Vertical cross-sectional view D3

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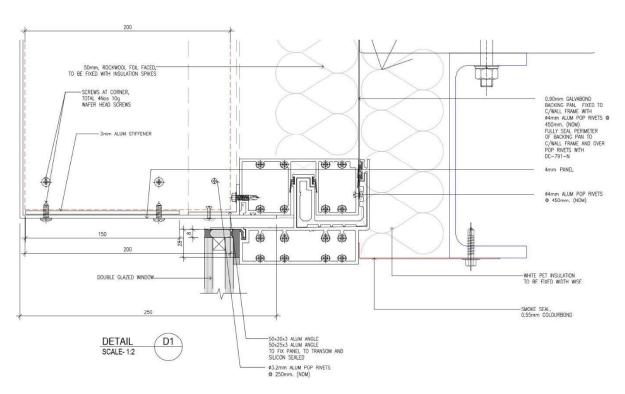


Figure 19 System assembly - Vertical cross-sectional view D1

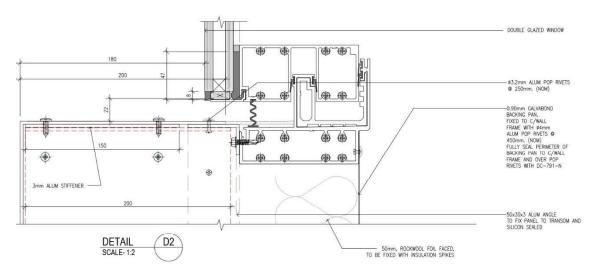


Figure 20 System assembly - Vertical cross-sectional view D2

Test standard: General accordance with ISO 13785-1:2002

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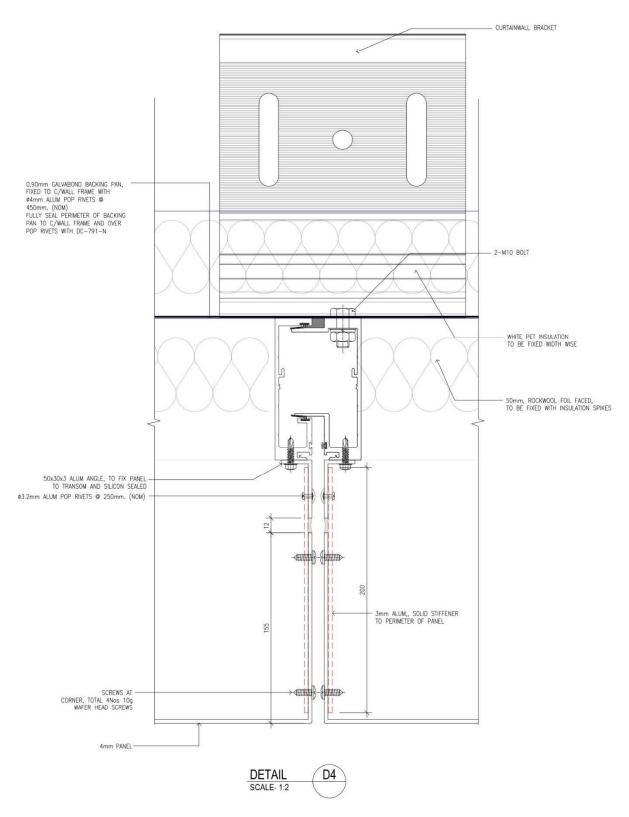


Figure 21 System assembly – Horizontal cross-sectional view D4

Test standard: General accordance with ISO 13785-1:2002

Job number: RTF230148



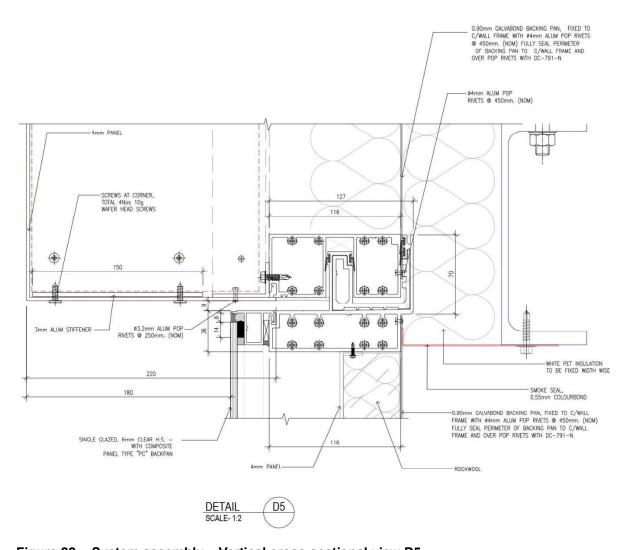


Figure 22 System assembly – Vertical cross-sectional view D5

Test standard: General accordance with ISO 13785-1:2002 Job number: RTF230148



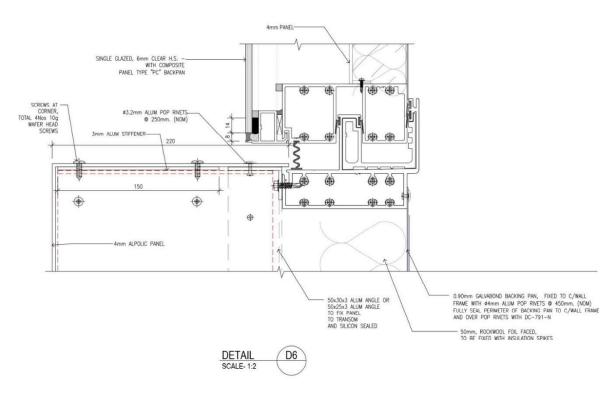


Figure 23 System assembly - Vertical cross-sectional view D6

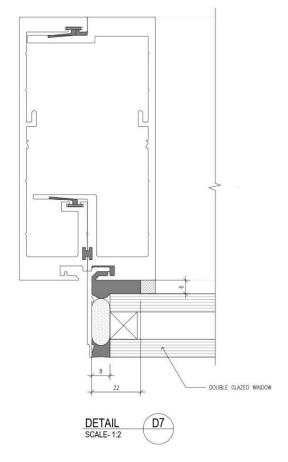


Figure 24 System assembly – vertical cross-sectional view D7

Test standard: General accordance with ISO 13785-1:2002

Job number: RTF230148



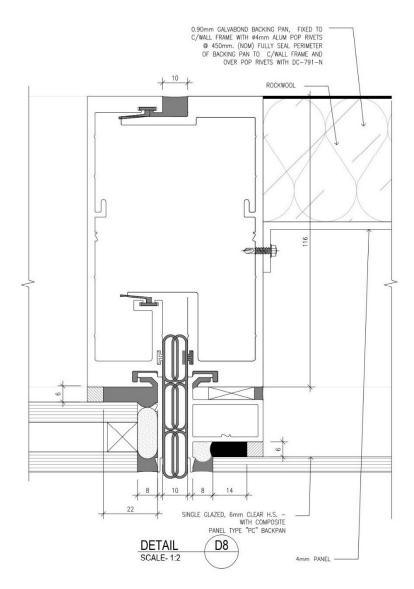


Figure 25 System assembly – vertical cross-sectional view D8

Test standard: General accordance with ISO 13785-1:2002 Job number: RTF230148



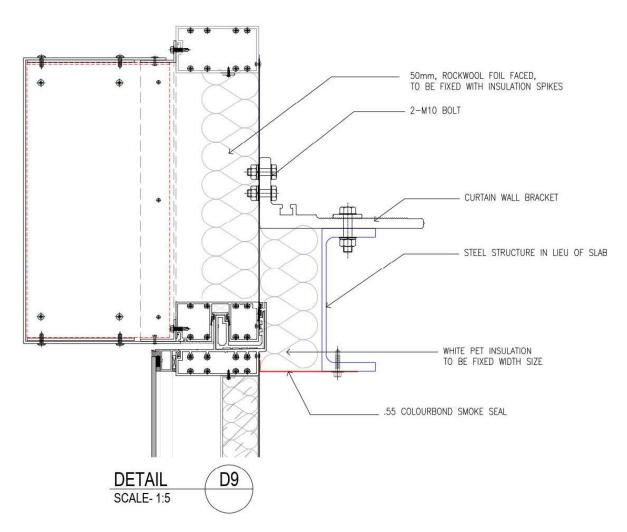


Figure 26 System assembly - vertical cross-sectional view D9

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Appendix B Photographs



Figure 27 The specimen (exposed side) before the reaction to fire test



Figure 28 The specimen (unexposed side) before the reaction to fire test

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Figure 29 The specimen 2 minutes 30 seconds into the test (burner output at 300 kW)



Figure 30 The specimen 5 minutes into the test (burner output at 300 kW)

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Figure 31 The specimen 7 minutes into the test (burner output at 300 kW)



Figure 32 The specimen 9 minutes 6 seconds into the test (burner output at 300 kW)

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Figure 33 The specimen 15 minutes into the test (burner output at 300 kW)



Figure 34 The specimen 21 minutes 45 seconds into the test (burner output at 300 kW)

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Figure 35 The specimen 27 minutes 46 seconds into the test (burner output at 300 kW)



Figure 36 The specimen 30 minutes 2 seconds into the test (burner off)

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Figure 37 The specimen 50 minutes into the test (burner off)

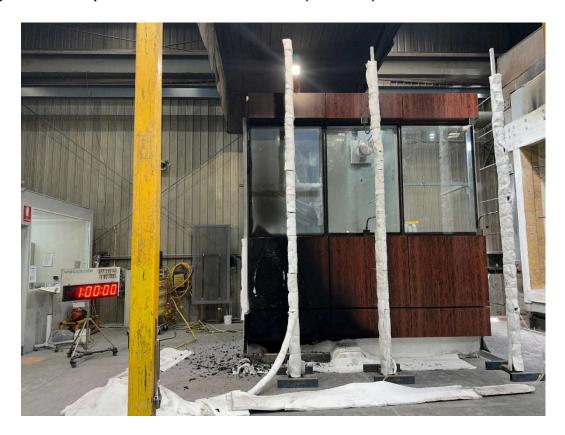


Figure 38 The specimen at end of test - exposed side





Figure 39 The specimen at end of test – unexposed side



Appendix C Chemical Analysis Results



UNSW RESEARCH INFRASTRUCTURE

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Test Report

Prepared by:

ANALYSIS OF CLADDING SAMPLES REF: UB8388

For

Company: Warrington Fire

Contact:

Date: 17 October 2023

Project No: 23197

Prepared by: Afsaneh Khansari Approved by: Dominic D'Adam



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Project No.: 23197

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Analysis of Cladding Samples REF: UB8388

1. SAMPLES

One plastic sachet containing two ACP cores was received for analysis. The samples were identified as follows:

CCL sample coding	Client sample coding
23197-1	Oak
23197-2	Silver

CCL has been asked to identify the polymer and the filler (s) in the samples by FT/IR, quantitate and identify the mineral filler in the samples and classify them in accordance with the ICA cladding scheme.

2. METHODOLOGY AND RESULTS

The aluminium metal was removed from the ACPs cladding polymer, and the flat surface of the polymer samples was abraded to remove any surface adhesive. The surface of each sample was analysed directly by FTIR. The FT-IR spectrum is presented in Figures 1-2.

The core of each sample was then ashed to determine its percentage mineral content (Table 1). If sufficient (>0.5 g) ash had been produced it was analysed for elemental composition by X ray fluorescence spectroscopy. Results are presented in Table 2.

Table 1 Ash content of samples.

Sample coding	Ash content (w/w%)
23197-1	39.5
23197-2	21.6

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Table 2 Elemental composition of 23197-1

Element Oxide wt.%	23197-1
Na ₂ O	0.45
MgO	79.26
Al ₂ O ₃	0.39
SiO ₂	4.87
P ₂ O ₅	0.12
SO ₃	0.26
K ₂ O	0.04
CaO	8.66
TiO ₂	2.24
V ₂ O ₅	0.01
Cr ₂ O ₃	<0.01
Mn ₃ O ₄	0.04
Fe ₂ O ₃	0.55
NiO	<0.01
CuO	<0.01
Zn0	0.01
Sr0	<0.01
ZrO ₂	<0.01
Ba0	0.09
HfO ₂	<0.01
PbO	<0.01
L.O.I.	ND

NOTE: (i) L.O.I.= loss on ignition at 1,050 °C.

(ii) ND = not determined



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3. CONCLUSIONS

The cladding sample #1 consisted of consisted of 45.3% magnesium hydroxide, 6.1% calcium carbonate, 4.8% other inert material and approximately 43.9% polyethylene/EVA copolymer.

The cladding sample #1, is classified as ICA category A.

The cladding sample#2 consisted of consisted of 21.6% inert material and approximately 78.4% polyethylene/EVA copolymer.

The cladding sample #2, is classified as ICA category A.

The ICA Classification assigned is correct as per the September 2020 revision of the ICA Guidelines.

The calculation for magnesium hydroxide content assumes that all magnesium found is present as the hydroxide. The calculation for calcium carbonate content assumes that all calcium found is present as calcium carbonate.

The reader is reminded that we can only analyse and classify the content of samples actually presented to us. We can offer no guarantee that this composition or classification is valid for cladding as a whole, because some types of cladding can be inhomogeneous, and a sample may not be representative of the cladding as a whole. Anyone using our results should consider these sampling issues and uncertainties before they generalise the results we present to anybody of cladding as a whole.

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Technical Officer
Chemical Consulting Laboratory
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17 October 2023



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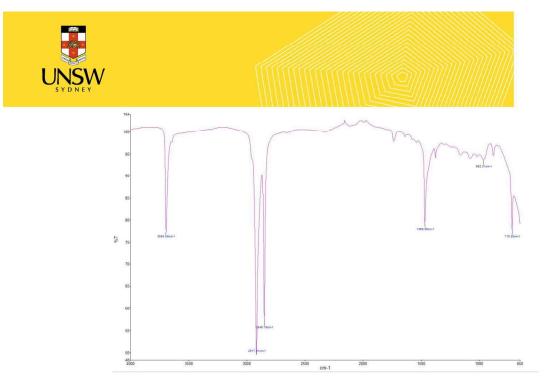


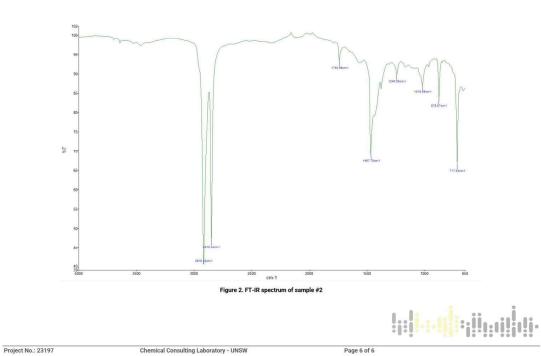
Figure 1. FT-IR spectrum of Sample #1

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